

Effects of Polymer Concentration and Molecular Weight on the Dynamics of Visco-Elasto-Capillary Breakup

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Capillary Breakup Extensional Rheometer (CABER)

Top and Bottom Cylinders: Diameter (D_0) = 6 mm

Initial height = 3 mm

Final height = 13.2 mm

Uses ~90 μL of sample

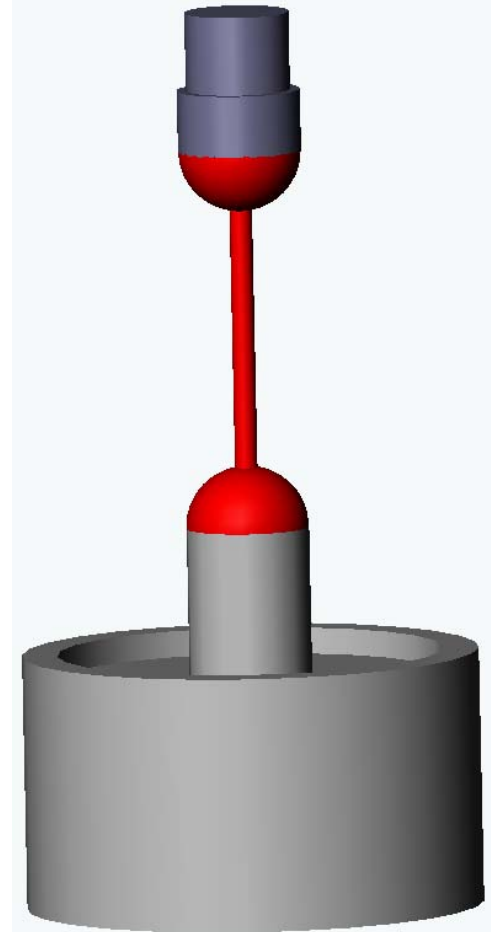
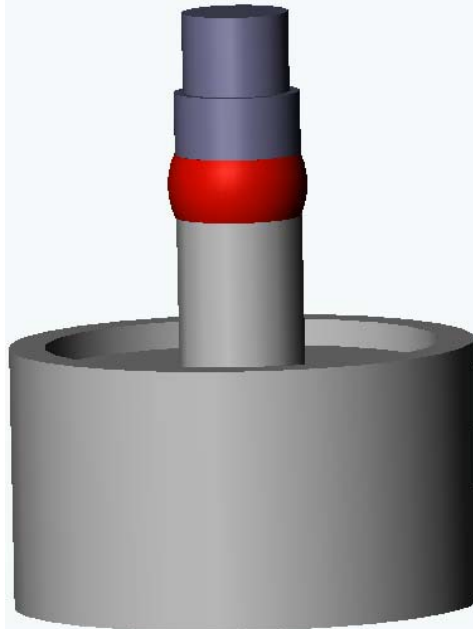
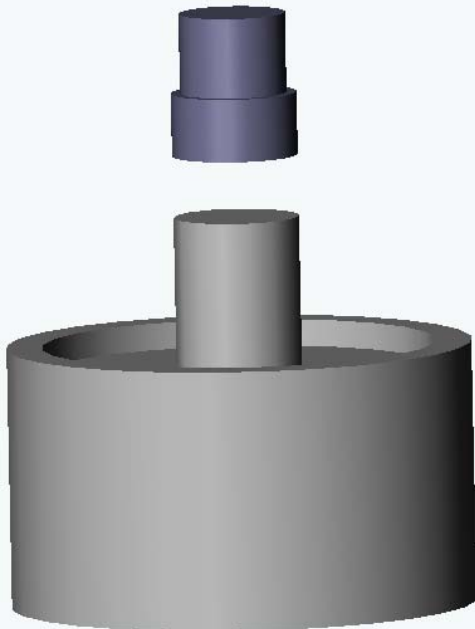
Time to open: 50 ms

Initial aspect ratio $\Lambda = \frac{H}{D_0} = .5$

Final aspect ratio = 2.2

Balance of

capillary, viscous, and
elastic forces



Balance of Stresses

If $F_{total} = 0$

$$\frac{\sigma}{R} = 3\eta_s \left(-\frac{2}{R} \frac{dR}{dt} \right) + (\tau_{zz} - \tau_{rr})$$

(capillary)

(viscous)

(elastic)

Normal stress differences:

$$\tau_p = [\tau_{zz} - \tau_{rr}] = \sum_i G_i f_i (A_{zz}^i - A_{rr}^i)$$

elastic moduli:

$$G = \frac{\eta_0 - \eta_s}{\lambda_z} \sum_i \frac{1}{i^{2+\nu}}$$

Initial conditions

- At early times, the viscous response of the solvent is not negligible for dilute polymer solutions

➔ The initial value of the axial stretch is chosen to fit the curve in order to obtain a shape as good as possible.

The polymeric stretch grows as

$$A_{zz}(t) = A_{zz}^0 e^{t/3\lambda_z}$$

- Other initial conditions are:

$$A_{zz}^{i \neq 1}(t = 0) = 1 \quad \text{and} \quad A_{rr}^i(t = 0) = 1$$

(undeformed material)

Ohnesorge and Deborah Numbers

The **Ohnesorge Number** evaluates the importance of viscous effects over inertial effects and, in our case, is defined by:

$$Oh = \frac{\eta_0}{\sqrt{\rho\sigma R}}$$

It can be seen as a Reynolds number:

$$Oh^{-2} = \frac{\rho v R}{\eta_0} \quad \text{where the capillary velocity is } v = \frac{\sigma}{\eta_0}$$

The **Deborah Number** is the dimensionless deformation rate computed as the ratio of the relaxation time of the fluid by the characteristic time of the experiment. It can be defined as:

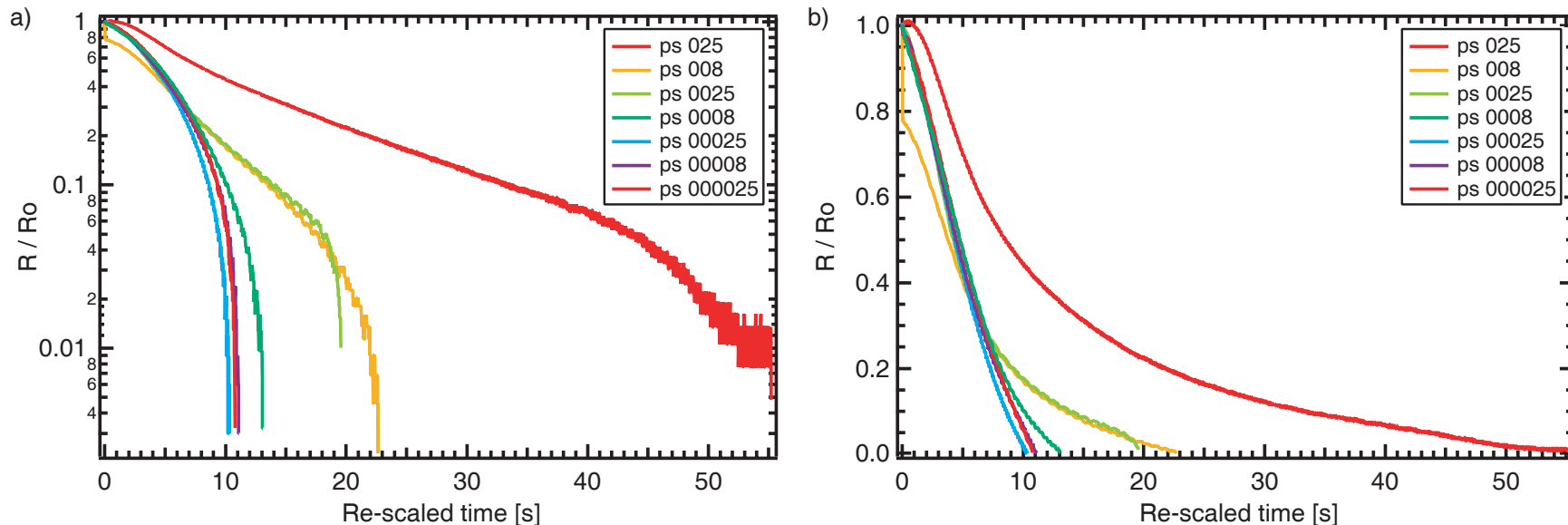
$$De = \frac{\lambda}{\sqrt{\rho R^3 / \sigma}}$$

The ratio of these two numbers is then an elasto-capillary number:

$$\frac{De}{Oh} = \frac{\lambda \sigma}{\eta_0 R}$$

Extensional Rheology: CABER experiments

Progressive dilution decreases time to breakup:

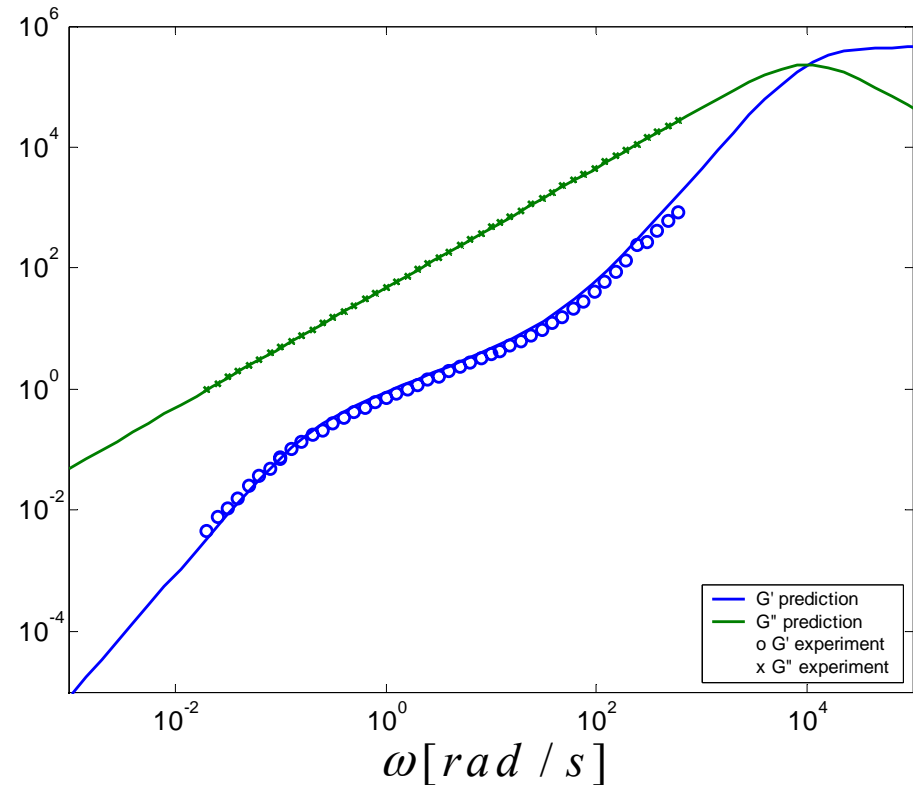
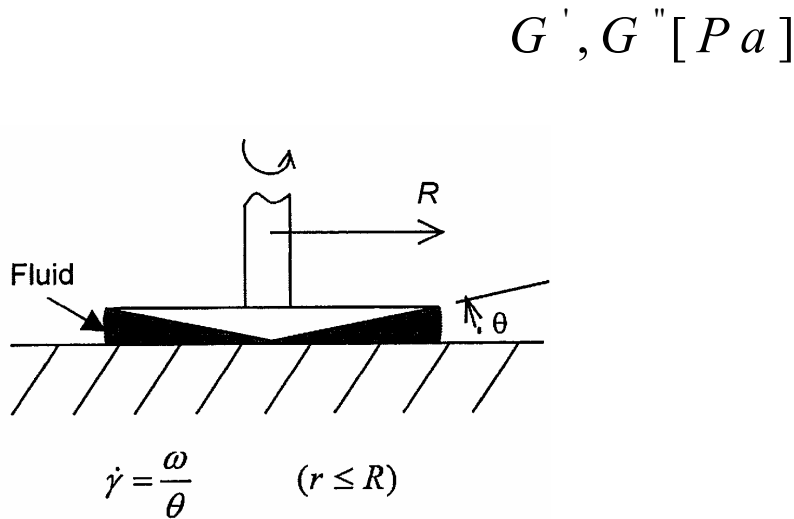


Compared to Kuhn Chain formula: $\lambda = \frac{1}{\zeta(3\nu)} \frac{[\eta]\eta_s M_w}{N_A k_B T}$ with $[\eta] = K \cdot M_w^{3\nu-1}$

Concentration [wt.%]	0.025	0.008	0.0025	0.0008	0.00025	0.00008	0.000025
Ratio c/c^*	0.273	0.0873	0.0273	0.00873	0.00273	0.000873	0.000273
Rel. Time Kuhn	3.14	3.14	3.14	3.14	3.14	3.14	3.14
Rel. Time CABER [s]	4.17	1.98	1.98	1.97	1.95	1.86	1.80

Shear Rheology: Cone and Plate Rheometer

From the data given by oscillatory shear flow with a cone and plate rheometer, one obtains the storage modulus G' and the loss modulus G'' . Fitting these data yields the relaxation time through Zimm theory.



Concentration [wt.%]	0.025	0.008	0.0025	0.0008
λ_{Fit} [s]	5.02	1.85	3.97	1.49

Governing equations: FENE-P model

Entov & Hinch, JNNFM 1997

The radius decreases according to

$$\dot{R} = -\frac{1}{2} \dot{\epsilon} R$$

$\dot{\epsilon}$: axial strain-rate of the axisymmetric extensional flow

Axial deformation

$$\dot{A}_{zz}^i = 2\dot{\epsilon} A_{zz}^i - \frac{f_i}{\lambda_i} (A_{zz}^i - 1)$$

Radial deformation

$$\dot{A}_{rr}^i = -\dot{\epsilon} A_{rr}^i - \frac{f_i}{\lambda_i} (A_{rr}^i - 1)$$

Finite extensibility: $L \sim M_w^{1-\nu}$

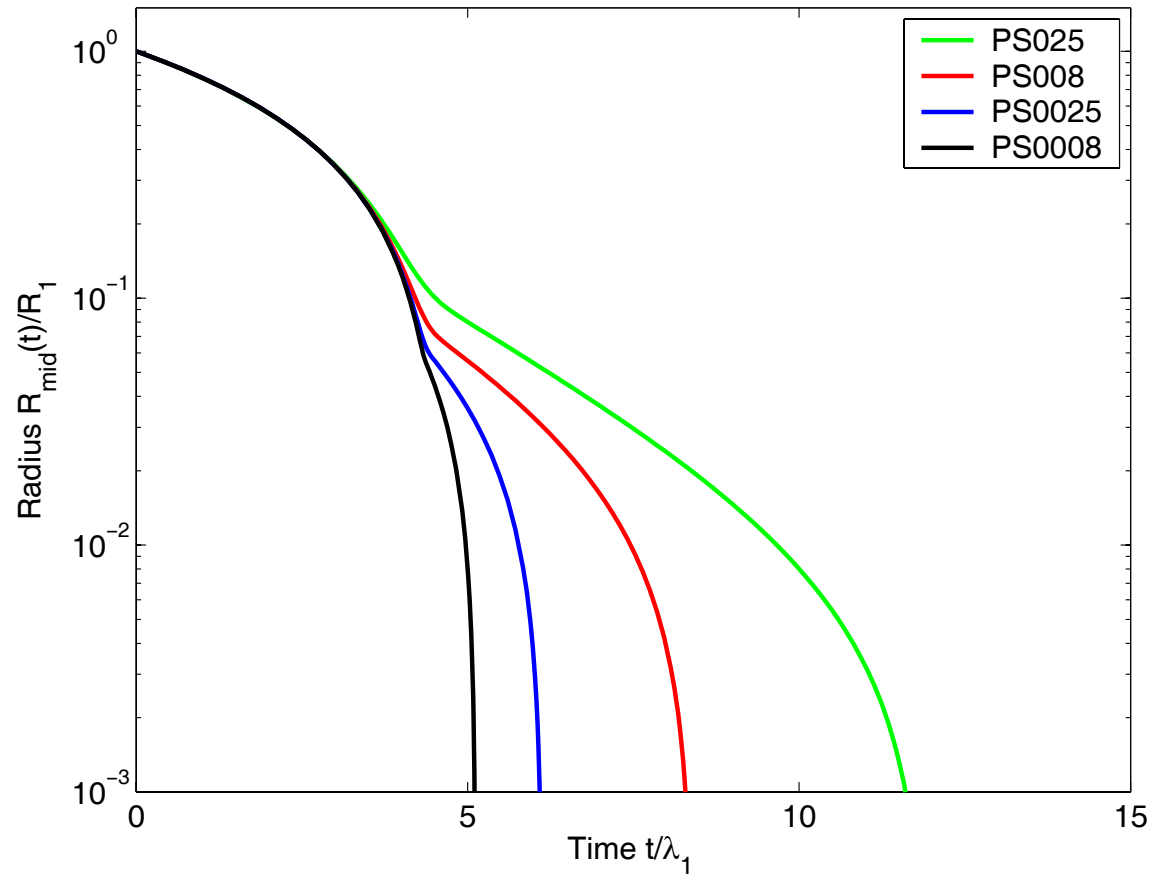
With relaxation times λ_i and FENE factors $f_i = \frac{1}{1 - \frac{tr A^i}{L_i^2}}$, $L_i = \frac{L}{i^\nu}$

Numerical Simulations

Decrease of the radius as a function of time.

Inputs of the simulation:

$$\eta_0, \eta_S, \lambda_{Zimm}, A_{zz}^0$$



Asymptotic Behaviors

1- Early viscous times:

For a strong surface tension with no elastic stress...

Stress balance:
$$\frac{\sigma}{R} = 3\eta_s \dot{\epsilon}$$



$$R = R_1 - \frac{\sigma}{6\eta_s} t$$

2- Middle elastic times:

Elastic stress grows. Viscous stress drops with the strain-rate. Balance between capillary pressure and elastic stress.

Assumption: $A_{zz}^i \gg 1 > A_{rr}^i$

The deformation is smaller than the finite extension limit: $A_{zz}^i \ll L_i^2 \quad (f_i = 1)$

Asymptotic Behaviors (2)

The radius decreases exponentially:

$$R(t) = R_1 \left(\frac{R_1 G(t)}{\sigma} \right)^{\frac{1}{3}} \quad \text{with} \quad G(t) = \sum_i G_i e^{-\frac{t}{\lambda_i}}$$

3- Late times limited by finite extension:

Viscous stress is the difference of large numbers. The system of equations is very stiff.

Balance capillary pressure/elastic stress:

$$\frac{\sigma}{R} = \sum_i G_i f_i \left(A_{zz}^i - A_{rr}^i \right)$$

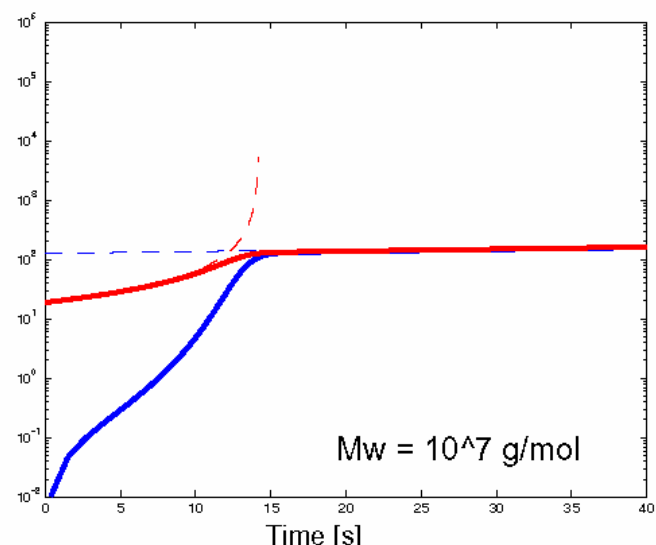
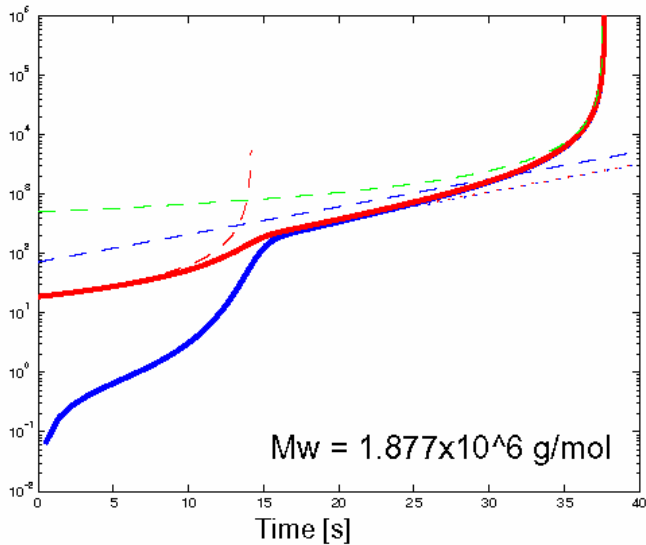
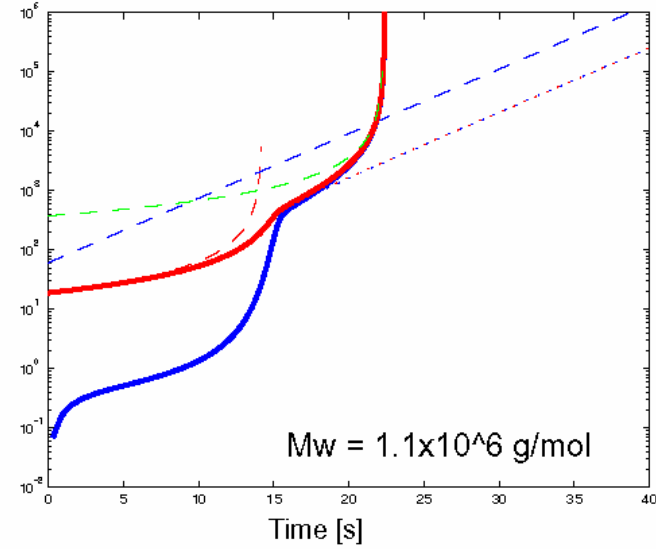
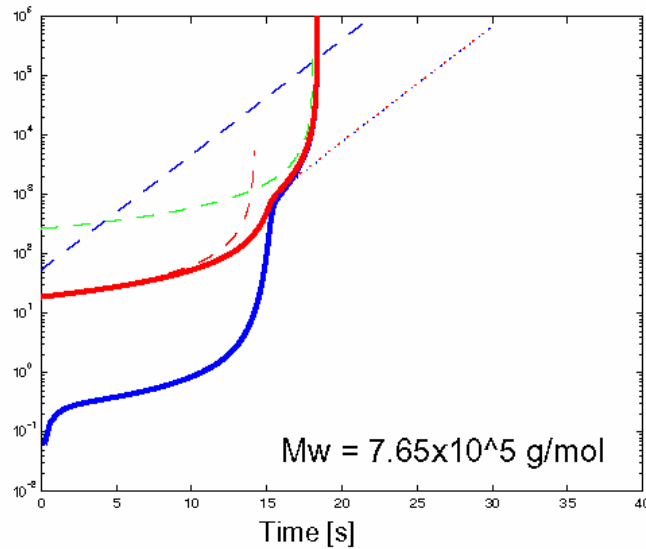
The FENE fluid is now behaving like a suspension of rigid rods, with an effective viscosity

$$\eta^* = \frac{2}{3} \sum_i G_i \lambda_i L_i^2$$

The decrease of radius is then linear:

$$R(t) = \frac{\sigma}{6\eta^*} (t_b - t)$$

Correspondence between numerics and asymptotes



- Capillary stress (numerical simulation)
- Elastic stress (numerical simulation)
- - - Capillary stress (infinite extensibility)
- - - Elastic stress (infinite extensibility)

- - - Visco-capillary balance
- - - Elasto-capillary balance
- - - Fully extended limit

Importance of Gravity: New Test Fluid (MV1)

Competition between gravitational and viscous forces: Bo/Ca

$$\frac{Bo}{Ca} = \frac{\rho g R_0}{\eta_0 \dot{\epsilon}} \longrightarrow \dot{\epsilon}_{sag} = \frac{\rho g R_0}{\eta_0}$$

$$De_{sag} = \frac{\lambda \rho g R_0}{\eta_0} = \frac{[\eta] M_w \rho g R_0}{\zeta (3\nu) N_A k_B T (1 + c[\eta])} \leq 0.5 \longrightarrow 1.3 \times 10^{-5} M_w^{1.59} \leq 0.5$$

$$M_w \leq 765000 \text{ g/mol}$$

$$M_w = 750000 \text{ g/mol}$$

Experimental Results:

Fluid	PS 025	MV1
Ratio c/c^*	0.273	0.50
Zero-shear viscosity [Pa.s]	49	53.5
Solvent viscosity [Pa.s]	45.5	48.5
Relaxation time Kuhn Chain [s]	3.14	0.78
Relaxation time by fitting with Zimm theory [s]	5.02	1.04
Relaxation time CABER [s]	4.17	1.09

Filament Thinning and Gravitational Sagging

Newtonian Fluid: Glycerol



$t = 0.01\text{s}$



$t = 0.06\text{s}$



$t = 0.11\text{s}$



$t = 0.18\text{s}$

New test fluid: MV1



$t = 0.01\text{s}$



$t = 9.00\text{s}$



$t = 18.00\text{s}$



$t = 27.00\text{s}$

Viscoelastic Fluid: PS 025



$t = 0.01\text{s}$



$t = 11.71\text{s}$

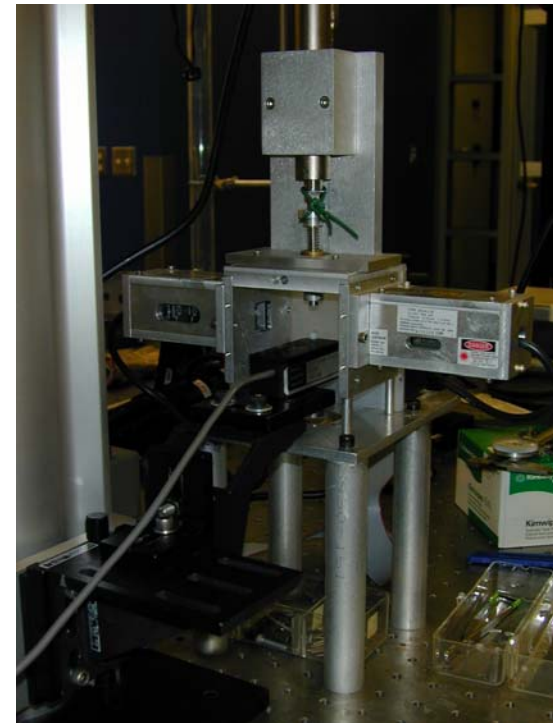
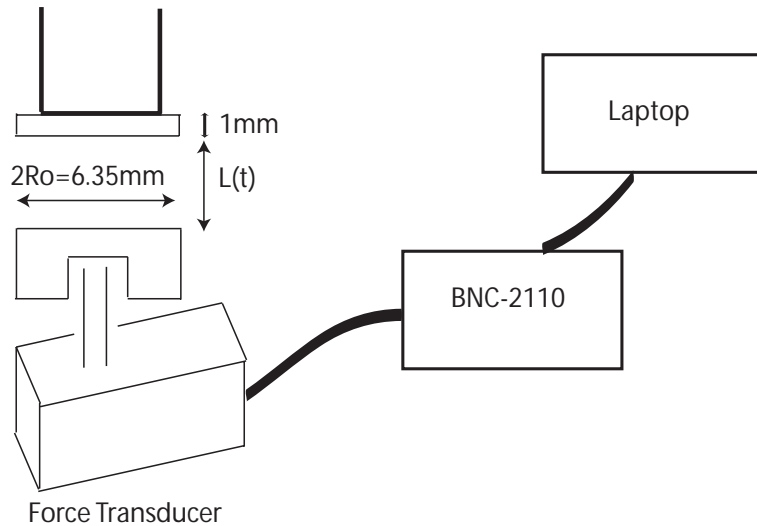


$t = 22.70\text{s}$

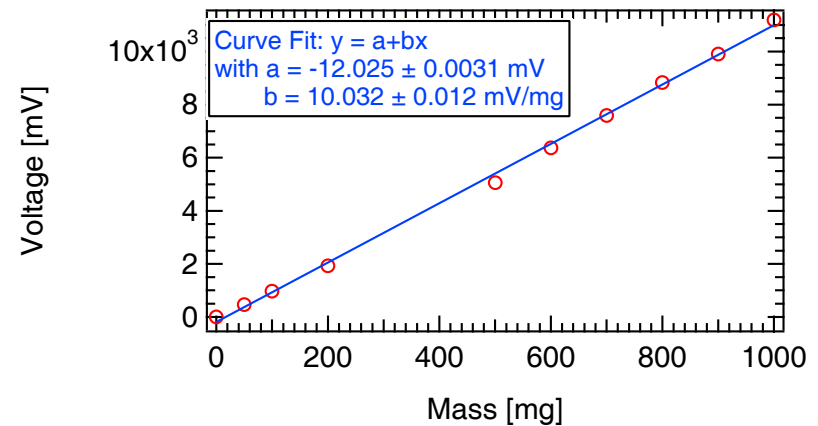


$t = 34.00\text{s}$

Force Transducer: Experimental Setup



Calibration:



Gain = 10 V/g

Maximal force = 0.01 N = 1 g

Force measured on the bottom plate of the CABER

Force Balance:

$$F_N = 3\eta_s \dot{\epsilon} \pi R^2(t) + \pi \sigma R(t) + \Delta \tau_p \pi R^2(t) - \rho g \pi \frac{R_0^2 L_0}{2}$$

Elongation:

$$\dot{\epsilon} = \frac{V_{plate}}{L} \rightarrow \dot{\epsilon}(0^-) = 15.38 s^{-1} \quad \text{and} \quad R(0^-) = R_0 e^{-3/4 \dot{\epsilon} t}$$

$$\rightarrow \begin{aligned} F_V(0^-) &= 2.07 \times 10^{-2} N \\ F_\sigma(0^-) &= 2.12 \times 10^{-4} N \end{aligned}$$

Stress Relaxation:

Visco-Capillary part: $\dot{\epsilon} = -\frac{2}{R} \frac{dR}{dt} = \frac{\sigma}{3\eta_s R} \rightarrow \dot{\epsilon}(0^+) = .158 s^{-1}$

$$F_N = 2\pi\sigma \left(R(0^+) - \frac{\sigma t}{6\eta_s} \right)$$

Force measured on the bottom plate of the CABER (2)

Elasto-Capillary part:

$$R(t) = R_i \left(\frac{GA_{zz}^0 R_i}{\sigma} \right) e^{-t/3\lambda}$$

$$F_V = \frac{2\pi\eta_s}{\lambda} R_i^2 \left(\frac{GA_{zz}^0 R_i}{\sigma} \right)^{2/3} e^{-2t/3\lambda}$$

$$F_\sigma = \pi\sigma R_i \left(\frac{GA_{zz}^0 R_i}{\sigma} \right)^{2/3} e^{-t/3\lambda}$$

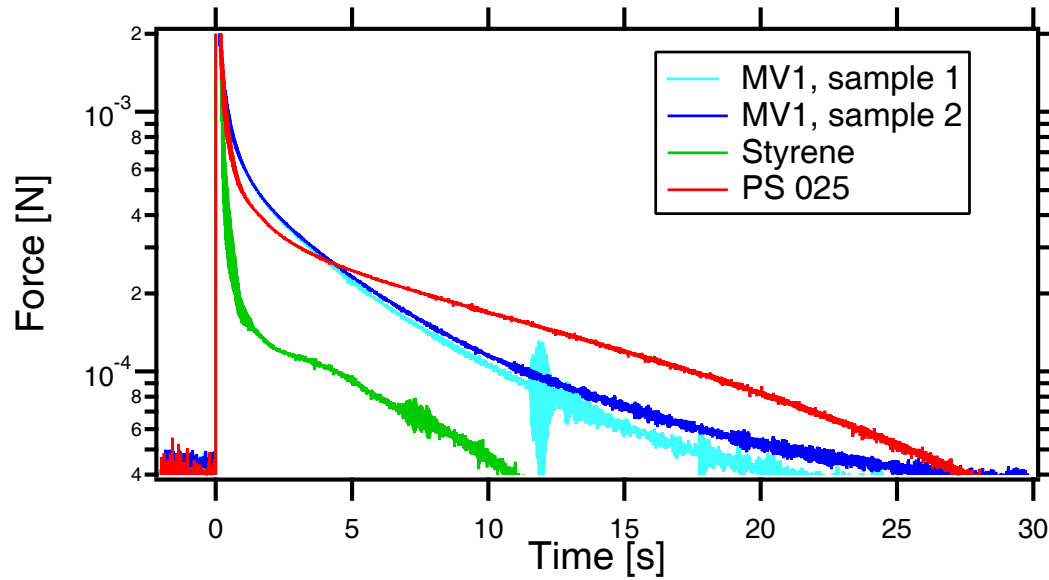
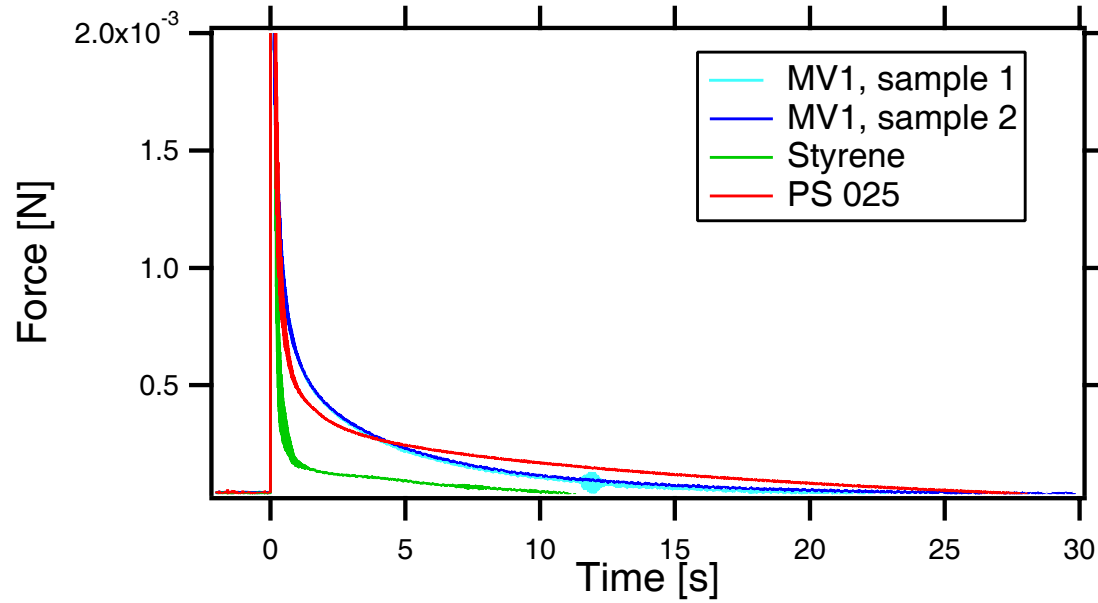
$$F_E = \pi GA_{zz}^0 R_i^2 \left(\frac{GA_{zz}^0 R_i}{\sigma} \right)^{2/3} e^{-t/3\lambda}$$

Measure of A_{zz}^0 : exponential fit of the force data $F_\sigma + F_E = \alpha e^{-\beta t}$

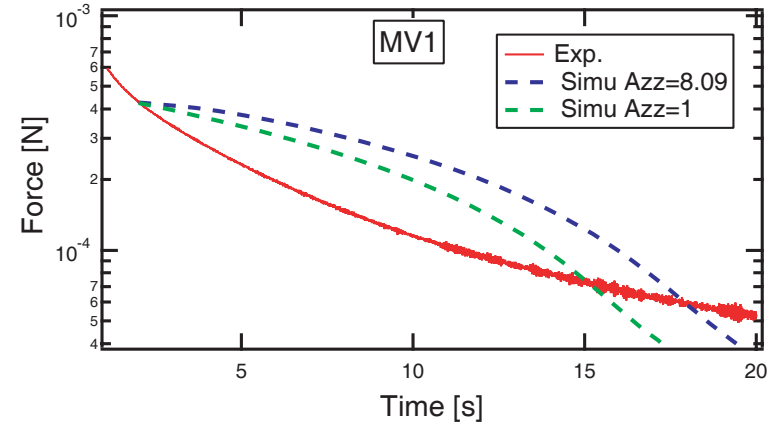
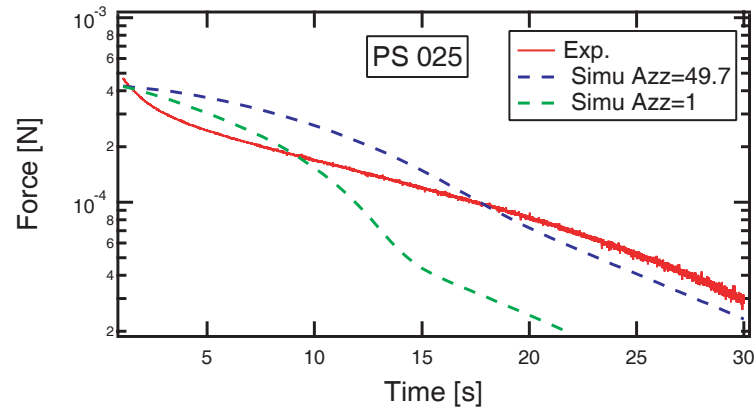
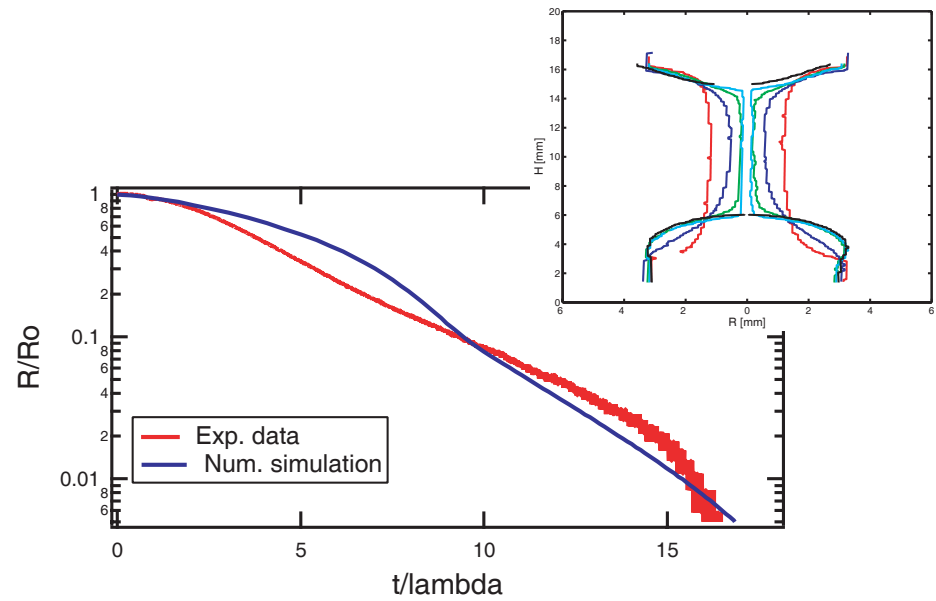
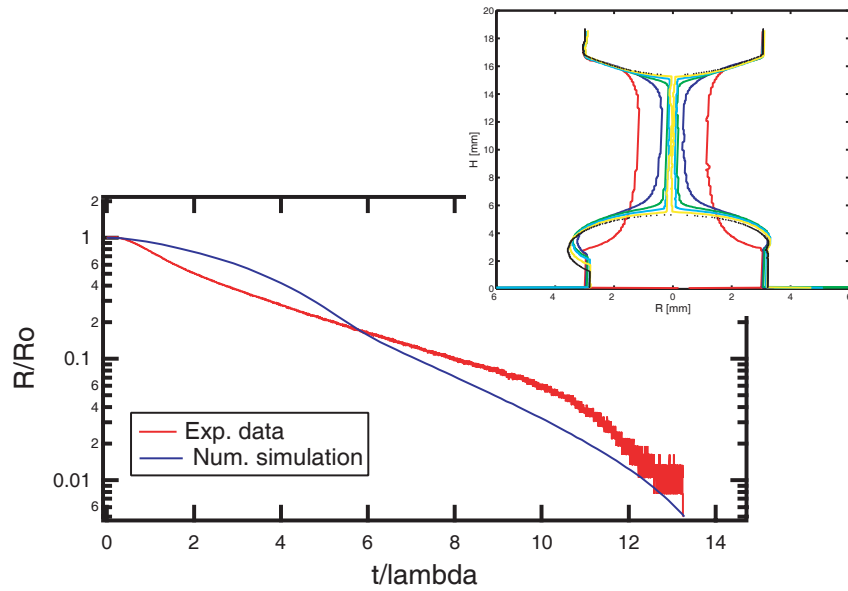
Fluid	PS 025	MV1
A_{zz}^0	49.7	8.09
λ [s]	4.83	1.82

Fluid	PS 025	MV1
F_exp [N]	4.64×10^{-4}	4.49×10^{-4}
F_num [N]	4.25×10^{-4}	4.26×10^{-4}
F_an [N]	4.25×10^{-4}	4.25×10^{-4}

Experimental Results

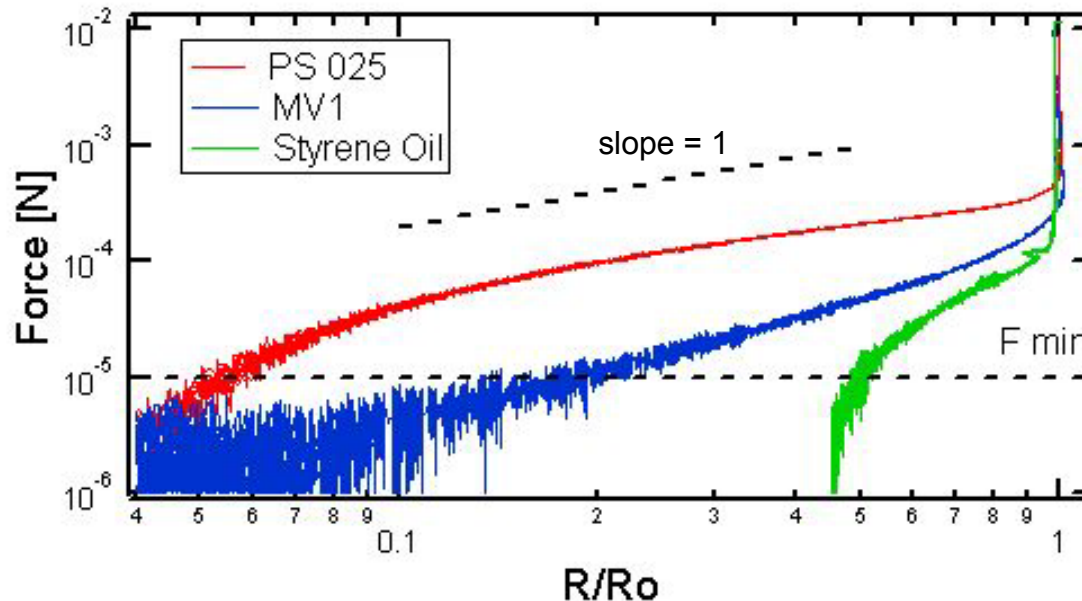


Comparison to the Simulations



Conclusion and Future Work

- Experimental and numerical demonstration of the concentration dependence for relaxation times.
- Breakdown of the necking in three asymptotic behaviors.
- Fabrication of a new viscoelastic fluid.
- Measure of the force on the bottom plate of the CABER: measure of Azz_0 .
- Simulation of the evolution of the force and comparison with experimental data.



QUESTIONS?